## PATENT SPECIFICATION

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## (54) HEAT EXCHANGE APPARATUS

(71)We, PULLMAN INCORPORATED, a Corporation organized and existing under the Laws of the State of Delaware, United States of America of 200 South Michigan 5 Avenue, Chicago, Illinois, United States of America, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed to be particularly de-10 scribed in and by the following state-

This invention relates to heat exchange

apparatus.

Exchanger reactors are used to simul-15 taneously heat and chemically react a process fluid passing through the exchanger reactor. One type of exchanger reactor includes a shell having a tube bundle positioned in the shell. The shell directs a 20 heating fluid about the tube bundle; and the tube bundle includes a plurality of tubes for passing the process fluid to be both heated and chemically reacted. The plurality of tubes of the tube bundle are packed with a catalyst, for example, for

react in the tubes. An example of an exchanger reactor is illustrated in U.S Patent 3,972,688 wherein gaseous or vaporized hydrocarbons are passed through a plurality of catalyst-containing tubes in order to produce carbon monoxide and hydrogen containing gases. In U.S. Patent

causing the process fluid to chemically

3,972,688, the catalyst tubes extend through a reactor housing and are position at least partly in a heating zone defined by the reactor housing. The portion of the tubes extending into the reactor housing is surrounded by an inner shielding wall

which is permeable to an outer shielding wall disposed within the reactor housing for defining a flow passage for the return of the heating gas after flow about the reactor tubes. U.S. Patent 3,958,951 illus-

trates a reformer furnace wherein a stream of hydrocarbon and steam is passed through the furnace tubes for producing a gaseous hydrocarbon and carbon monoxide mixture.

Of course, exchanger reactors are usable

in many different applications in addition to those mentioned, which are described merely to provide examples of such use.

According to this invention heat exchange apparatus comprises:

a generally cylindrical hollow shell assembly comprising a main heating chamber, a shell inlet chamber and a shell outlet chamber arranged therein such that a heating fluid is flowable through said shell inlet chamber into said main heating chamber and outwardly through said shell outlet chamber;

a tube bundle assembly mounted in and separate from said shell assembly;

inlet means and outlet means for directing a process fluid to be heated through said tube bundle assembly;

said tube bundle assembly comprising (a) a tube inlet chamber comprising a generally hemispherically shaped inlet section attached to an inlet tube sheet extending transversely across said inlet section and connected to said inlet means, (b) a tube outlet chamber comprising a generally hemispherically shaped outlet section attached to an outlet tube sheet extending transversely across said outlet section and connected to said outlet means; (c) a plurality of tubes which extend between said inlet tube sheet and said outlet tube sheet so as to be positioned in said shell main heating chamber; and (d) expansion means positioned between said inlet means and said inlet chamber for providing 85 relative movement between said shell assembly and said tube bundle assembly;

a radial flow inlet distributor means positioned between said shell inlet chamber and said main heating chamber for distributing heating fluid radially inwardly from said shell inlet chamber into said main heating chamber; and a radial flow outlet distributor means positioned between said shell outlet chamber and said main heating chamber for distributing heating fluid radially outwardly from said main heating chamber into said shell outlet chamber.

The invention may be performed in

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QΩ

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various ways and one specific embodiment will now be described by way of example with reference to the accompanying drawings in which:-Figure 1 is a sectional view of an exchanger reactor; Figure 2 is a sectional view taken along line 2—2 of Figure 1 illustrating schematically the plurality of tubes of the 10 tube assembly; and Figure 3 is a detailed view of a catalyst retainer mounted in each of the tubes of the tube bundle. Referring to the drawings, the letter E 15 generally designates the exchanger reactor of the preferred embodiment of this invention. The exchanger reactor E includes a shell assembly 10 which houses a tube bundle assembly 11. Basically, the shell assembly 10 includes a shell inlet chamber 12a, a main heating chamber 12b and a shell outlet chamber 12c. A heating fluid is directed through the shell inlet chamber 12a into the main heating chamber 12b and 25 outwardly through the shell outlet chamber 12c. The tube bundle assembly 11 includes a tube inlet chamber 14a, a plurality or bundles of tubes 14b (one representative tube is shown in Figure 1) and a tube outlet chamber 14c. A process fluid to be heated is directed through the tube inlet chamber 14a into the plurality of tubes 14b and outwardly through the tube outlet chamber 14c. The heating fluid, which may 35 approach a high temperature near the failure point of the high temperature metals utilized, transfers heat through the plurality of tubes 14b to the process fluid flowing through the plurality of tubes 14b. 40 The plurality of tubes 14b are filled, such as with catalyst, so that the process fluid flowing through the plurality of tubes is subjected to a chemical reaction such as cracking or reforming in order to produce 45 a product which is different in chemical composition from the process fluid entering the reactor. Referring to Figure 3, the bottom end of each tube has a catalyst retainer means 14d mounted therein to 50 hold the catalyst. The catalyst retainer means 14d is a perforated, conically-shaped element mounted in the bottom tube end by welding and having openings such as 14e to pass the reacted process fluid. One 55 example of such use of the exchanger reactor E is in the production of hydrogen-rich gas wherein hydrocarbon feed is passed through steam reforming catalyst-filled tubes of the tube bundle assembly which are heated by high temperature heating fluid at 1600-1900 °F and at a pressure of

300-1000 psi. The exchanger reactor E

can also be used as a heat exchanger by

65 a catalyst.

utilizing the plurality of tubes 14b without

The shell assembly 10 includes a generally hemispherically-shaped, hollow top head 15 which includes an outer housing portion 15a which terminates in its upper end in an opening 15b formed by 70 ring 15c and at its lower end in a flange ring 15d. The interior of the head 15 includes an inside liner 15e of suitable material having an insulation layer 15f located between the inside liner 15d and 75 outer housing portion 15a. The inside liner 15e has a hemispherical configuration identical to that of the exterior housing portion 15a thereby creating a domeshaped interior space 16. 80 The shell assembly 10 further includes a main, generally cylindrical, hollow housing section 17 including outer housing 17a which is attached to the top head flange ring 15d by an upper flange ring 17b. The 85 outer housing 17a has a lower opening 17c having an inlet nozzle 17d welded thereto for connection to a process line for receiving a heating fluid. The outer housing 17a includes an upper opening 17e 90 having an exit nozzle 17f welded thereto for transferring outwardly of the main housing section 17 the heating fluid after it has been used to transfer heat to the tube bundle assembly 11. The main housing section 17 further includes a main, inner cylindrical lining 18 positioned within the outer housing 17a and spaced therefrom in order to receive a suitable refractory insulating material 19. 100 The main inner lining 18 further includes an inlet liner 18a positioned within the inlet nozzle 17d and an outlet liner 18b positioned within exit nozzle 17f in order to contain insulation refractory material, 105 also. The insulation refractory material can be a bubble aluminium such as carborundum "ALFRAX BI No. 57" or other suitable refractory material (ALFRAX is a Trade Mark). 110 A bottom head 20 of a generally hemispherical configuration is welded at 20a to the main housing section 17. The bottom head 20 includes a generally hemispherical outer housing 20b that has a nozzle 20c 115 welded thereto. The tube bundle assembly 11 includes an inlet tubular section or channel 25 terminating at its upper end in flange ring 25a and extending longitudinally inwardly into 120 the interior space 16. A suitable adapter or neck such as 26 is mounted onto the top head ring 15c and channel flange ring 25a by bolt assemblies to connect the tube 125 bundle assembly 11 to a source of process gas or other fluid. An expansion joint 25b of any well-known variety is mounted in the channel 25 such that the channel is

floating to provide for relative movement

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between the shell 10 and tube bundle

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assembly 11. A dome-shaped or hemispherical inlet section 27 is mounted onto the bottom end of the channel 25. The inlet section 27 is attached to tube sheet 28 by welding or other means. The tube sheet 28 includes a plurality of openings through which the upper ends of the plurality of tubes 14b extend. The dome-shaped inlet section 27 cooperates with the tube sheet 10 28 to form the tube inlet chamber 14a. The channel 25 and inlet section 27 is of sufficient size to allow a man to physically enter, remove and reload catalyst from the plurality of tubes 14b.

15 A circular insulation barrier or wall 30

extends transversely across the upper end of the main housing section liner 18 parallel to the upper tube sheet 28 but spaced therefrom a distance d. The spacing 20 of the entrance insulation wall a distance d away from the tube sheet 28 creates a void to at least eliminate some undesirable heat transfer. The insulation wall 30 is a castable refractory which is constructed prior to installation and includes a plurality of openings through which the plurality of tubes 14b extend. The insulation wall 30 is mounted at the top of the main housing section 17 with its circumferential edge positioned against the inside liner 18. A circular metal plate 31 is mounted adjacent to and supports the insulation wall 30 and thus extends transversely across the upper main housing section 17, also. The plate 31 35 is not attached to the liner 18, but does fit tightly against it.

The plurality of tubes 14b extend downwardly through the tube sheet 28, the spaced, insulation wall 30, the plate 31, through the main heating chamber 12b and terminates in a tube sheet 32 which is welded or otherwise attached to a domeshaped or hemispherical outlet section 33. Tie rods 29 (one representative tie rod is shown in Figure 1) extend downwardly from attachment to tube sheet 28 to a bolted attachment to circular plate 34.

The hemispherical outlet section 33 is connected to an outlet channel 33a which 50 extends downwardly onto a ledge 20e of the nozzle 20c and is welded thereto. An interior liner sleeve 35 is spaced from the channel 33a and nozzle 20c in order to contain an annular layer 36 of castable 55 refractory. A plurality of radially extending gussets 36a are attached to the outside hemispherical section 33 and extend into engagement with the top rim of the nozzle 20c in order to aid in the support of the 60 complete tube bundle assembly 11. The space between hemispherical section 33 and the head housing 20a is filled with insulation material. The tube sheet 32 cooperates with the hemispherical section 33 65 to form the tube outlet chamber 14c.

A circular insulation barrier or wall 37 extends transversely across the lower end of the main housing section liner 18 parallel and immediately adjacent to and supported by the bottom tube sheet 32. The insulation wall 37 is a castable refractory which is formed prior to installation and includes a plurality of openings through which the plurality of tubes 14b extend.

The circular plate 34, which is attached to the tie rods 29, is mounted against but is not attached to the inside liner 18 and is spaced from the insulation wall 37 a distance d'. The circular plate 34 includes a plurality of holes through which the plourality of tubes 14b extend. The separation distance d' between the wall 37 and the plate 34 is to prevent at least some undesirable heat loss.

85 The bottom tube sheet 32 cooperates with the top tube sheet 28 and tie rod attachment plate 34 to provide the primary support for the plurality of tubes 14b. The plurality of tie rods 29 are spaced, as viewed in section in Figure 2, for supporting the baffle structure to be discussed hereinafter. The pattern for the tubes is illustrated schematically in Figure 2. Thus one of the plurality of tubes 14b is actually centered at each intersection point shown in the pattern of lines illustrated in Figure 2. The geometric configuration for the tubes may be described as being triangular. 100 The purpose of the triangular configuration is to provide an efficient tube surface area for exposure to radial flow of the heating fluid.

A central tie rod 29a extends from the centre of the upper tube sheet 28 to the centre of tie rod plate 34. However, there are no tubes immediately adjacent to the central tie rod thus providing a longitudinally extending void space 29b along the length of the plurality of tubes 14b between barriers 44, to be described hereinafter. The purpose of the void space 29b is to eliminate tubes which would not receive as much heat as the other tubes and thus would not expand to the same extent as do the other tubes.

A radial flow distributor means generally designated by the number 40 and including annular wall distributor 41 having angularly spaced openings therethrough is positioned between the shelf inlet chamber 12a and the main heating chamber 12b for initially distributing heating fluid radially inwardly from the shell inlet chamber 12a into the main shell heating chamber 12b. The annular wall 41 is welded or otherwise attached to the transversely extending plate 34 and to an annular flow director or baffle 42 having a central opening 42a. The plurality of tubes

14b extend through a portion of the baffle 42 adjacent opening 42a and through the opening 42a itself. The position of baffle 42 is shown schematically in Figure 2. The 5 flow director or baffle 42 fits tightly against the main heating chamber liner 18. The circumferentially-shaped shell inlet chamber 12a is formed by circular plate 34, annular distributor 41 and annular plate 42 10 in cooperation with the liner 18, which forms a circumferential or annular inlet space which receives the heating fluid from nozzle 17d. Thus heating fluid enters through opening 17c, expands into the 15 annular inlet space and is then distributed radially inwardly through the openings in the annular distributor 41 into raidal flow engagement with the plurality of tubes 14b. The heating fluid then flows down-20 stream in the direction of arrow 43 and flows radially outwardly on the downstream side of the flow director 42 and around a second, circular flow director or baffle 44. The flow director 44 is a circular 25 barrier or wall having a diameter approximately equal to the diameter of the plurality of tubes 14b of the tube bundle and having a plurality of openings through which each of the tubes 14b extend to 30 thereby prevent flow across the baffle within the space occupied by the tubes The circular flow director 44 cooperates with annular flow director 42 to cause the fluid to flow radially outwardly after pass-35 ing through the opening 42a in the annular flow director 42. Annular flow directors 45, which are structurally identical to flow director 42, and the circular flow directors 44 are alternately spaced along the length 40 of the main heating chamber 12b in order to cause the flow of heating fluid to flow in alternating radial directions (with respect to the longitudinal axis 50 of the tube bundle assembly 11 and shell assembly 10) 45 across the plurality of tubes 14b, which causes efficient heat transfer from the heating fluid to the process fluid flowing through the tubes. Due to the high temperatures of the heating fluid, the utiliz-50 ation of alternating radial flow is very important to uniform heat distribution and temperature gradient along the tube bundle. The distance between baffles 44 and 45 and the relative inside diameter 45a 55 and outside diameter of baffle 44 may vary along the length of the axis 50. A radial flow outlet distributor means

generally designated by the number 46 in-

director 48 and to the plate 31 by welding

distributor 47 has a plurality of angularly

spaced openings therein in order to pass

cludes an annular distributor 47 which is

60 attached to the uppermost annular flow

or other suitable means. The annular

65 radially outwardly heating fluid into the

annular space or shell outlet chamber 12c formed between the distributor 47 and the inside liner 18. The heating fluid then flows outwardly of shell outlet opening 17e thus exiting the exchanger reactor E. In operation and use of the exchanger reactor E, it may be necessary from time to time to remove the tube assembly 11. In order to remove the tube assembly 11, the adapter 26 is first removed by releasing the 75 bolt connections of adapter 26 to channel flange ring 25a and to shell head ring 15c. The head 15 can then be lifted off the main shell section 17 (after release of the connection of flanges 15d and 17b). Next, 80 the inside liner 35 in lower head 20 is removed and the insulation material 36 is chipped away to expose the welded connection between the channel 33a and the nozzle 20c. This weld is then broken 85. which frees the entire tube assembly 11 for removal from the top. The entire shell assembly 10 is water jacketed as shown schematically by jacket shell 51 to reduce the operating temperature of the shell so that more common metals can be used in shell construction The jacket shell 51 extends from a position above tube sheet 28 to a position below tube sheet 32. 95 As previously mentioned, a preferred use of the exchanger reactor E is to carry out a primary reforming process to produce a hydrogen-rich gas or synthesis gas. In the primary reforming process, hydro-100 carbons are contacted with steam in the presence of steam reforming catalyst. Thus, in the preferred use, a gaseous hydrocarbon, or liquid hydrocarbon which can be gasified, is passed together with 105 steam through the tube assembly 11 and more particularly through the plurality of tubes 14b which are filled with a steam reforming catalyst 14f, such as a commercial nickel catalyst, i.e. nickel on a solid 110 support. The hydrocarbon stream enters the tubes 14b at temperatures less than 540 °C (1000 °F) and are heated such that the outlet temperatures are maintained at between 730 °C and 925 °C. The pressure in the steam reforming process may range from atmospheric pressure to 75 atmospheres (1100 psi) and preferably reformed gas or synthesis gas is then followed by secondary reforming and other process 120 steps to form a synthesis gas which may be used to produce ammonia, methanol or other products. Such process steps are described in U.S. Patent 3,119,667 Unlike conventional primary reforming where the catalyst filled tubes are in a fired

furnace and the endothermic heat of

in the radiant zone of the furnace, the

reaction is supplied by combustion of fuel

endothermic heat of reaction is supplied to 130

	effluent stream from the secondary
	reformer which has an outlet temperature
	between 870 °C and 1075 °C. This stream
5	is directed through the shell inlet chamber
	12a into the main heating chamber 12b an
	outwardly through the shell outlet chambe
	12c. It is understood that the pressures of
	the stream in the tubes 14b and the stream
10	directed through the shell have a differen-
	tial pressure of 10 to 100 psi although sub
	stantial pressures are maintained in the ex-
	changer reactor E. This use has special
	application in an ammonia process.
15	The exchanger reactor of the preferred
	embodiment of this invention is used as ar
	exchanger reactor in various chemical pro-
	cesses. The exchanger reactor is provided
•	for transferring heat from a high tempera-
20	ture heating fluid to a process fluid flowin
	through a plurality of tubes. The exchange
	reactor includes a generally cylindrical
	hollow shell assembly and a tube bundle
~-	assembly which is mounted in the hollow
25	shell assembly and cooperates therewith to
	provide a main shell heating chamber, a
	shell inlet chamber and a shell outlet
	chamber for directing a heating fluid
30	through the shell inlet chamber into the
50	main heating chamber and outwardly through the shell outlet chamber. The tube
	bundle assembly mounted in the shell
	assembly includes a plurality of tubes
	positioned in the shell main heating
35	chamber. The tube bundle assembly in-
	cludes a tube inlet chamber for passing a
	process fluid to be heated into the plurality
	of tubes and a tube outlet chamber for
	passing the process fluid outwardly of the
40	exchanger reactor. A first annular
	distributor is positioned between the shell
	inlet chamber and the main shell heating
	chamber for directing the heating fluid
	radially inwardly into contact with the
45	plurality of tubes positioned within the
	main heating chamber. A second annular
	distributor is positioned between the shell
	outlet chamber and the main heating
50	chamber for transferring the heating fluid
50	radially outwardly from the main heating
	chamber after such heating fluid has
	travelled in alternating radially directions
	(relative to the common longitudinal axis
55	of the tube bundle assembly and the shell
	assembly) along the tube assembly and transferred heat thereto. The plurality of
	tubes of the tube bundle assembly may be
	filled with a catalyst such that the process
	fluid flowing therethrough is chemically
50	reacted for producing a product such as a
-	synthesis gas.
	WHAT WE CLAIM IS:—
	1. Heat exchange apparatus comprising:
	a generally cylindrical hollow shell

assembly comprising a main heating

the exchanger reactor E by using the

5 chamber, a shell inlet chamber and a shell outlet chamber arranged therein such that a heating fluid is flowable through said shell inlet chamber into said main heating chamber and outwardly through said shell 70 outlet chamber: a tube bundle assembly mounted in and separate from said shell assembly; inlet means and outlet means for directing a process fluid to be heated 75 through said tube bundle assembly; said tube bundle assembly comprising (a) a tube inlet chamber comprising a generally hemispherically shaped inlet section attached to an inlet tube sheet 80 extending transversely across said inlet section and connected to said inlet means, (b) a tube outlet chamber comprising a generally hemispherically shaped outlet section attached to an outlet tube sheet 85 extending transversely across said outlet section and connected to said outlet means; (c) a plurality of tubes which extend between said inlet tube sheet and said outlet tube sheet so as to be positioned in said 90 shell main heating chamber; and (d) expansion means positioned between said inlet means and said inlet chamber for providing relative movement between said shell assembly and said tube bundle assembly; a radial flow inlet distributor means positioned between said shell inlet chamber and said main heating chamber for distributing heating fluid radially inwardly from said shell inlet chamber into said 100 main heating chamber; and a radial flow outlet distributor means positioned between said shell outlet chamber and said main heating chamber for distributing heating fluid radially outwardly from said main heating chamber into said shell outlet chamber. Apparatus as claimed in claim 1 wherein said radial flow inlet distributor means comprises a plate extending transversely of said shell assembly, an annular flow baffle having a central opening and an annular flow distributor mounted about said plurality of tubes and having openings therein for directing heating fluid radially inwardly from said shell inlet chamber into said main shell heating chamber. 3. Apparatus as claimed in claim 1 or claim 2, wherein said radial flow outlet distributor means comprises a plate extending 120 transversely of said shell assembly, an annular flow baffle having a central opening and an annular flow distributor mounted about said tubes and having openings therein for directing heating fluid 125 radially outwardly from said main heating chamber into said shell outlet chamber.

4. Apparatus as claimed in any one of the preceding claims, comprising an insu-

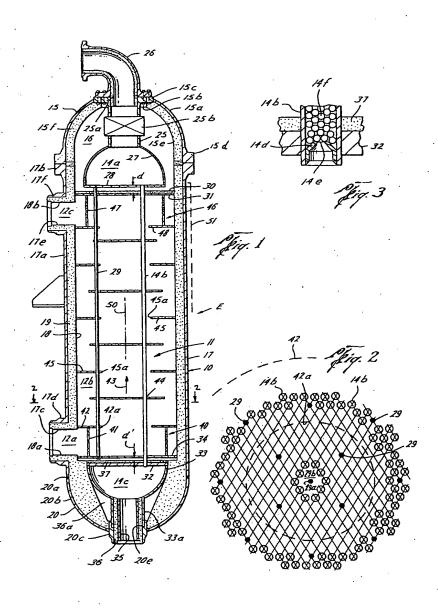
lation wall extending substantially parallel

	to said inlet tube sheet but spaced there- from and forming a dome-shaped interior space, said insulation wall having holes therein through which said plurality of	7. Apparatus as claimed in any one of the preceding claims, comprising catalyst retainer means mounted in one end of each tube of said tube bundle assembly for	
	tubes extend. 5. Apparatus as claimed in any one of the preceding claims, comprising an insu-	retaining a catalyst therein.  8. Apparatus as claimed in claim 2, comprising tie rods extending from said in-	35
	lation wall extending substantially parallel to and supported by said outlet tube sheet,	let tube sheet to said plate of said radial flow inlet distributor means.	
10	said insulation wall having holes therein through which said plurality of tubes extend.	. Apparatus as claimed in any one of the preceding claims, including a lining positioned within said shell assembly con-	. 40
	6. Apparatus as claimed in claim 2, comprising a plurality of first flow directors which are annular having a	taining a refractory insulating material.  10. Apparatus as claimed in any one of the preceding claims, including a water	45
13	central opening substantially as large as said central opening in said annular flow baffle in said radial flow distributor means	jacket external of said shell assembly which extends from above said inlet tube sheet to below said outlet tube sheet.	
20	and positioned at spaced intervals in said main heating chamber; and a plurality of second flow directors which are circular having openings therein through which said	11. Heat exchange apparatus substantially as hereinbefore described with reference to and as illustrated in the accompanying drawings.	50
	individual tubes extend and being positioned between said first flow directors		
25	in said main heating chamber, said first and second flow directors causing the heating fluid to flow through said main heating chamber in alternating radial	WILSON, GUNN & ELLIS, Chartered Patent Agents, 41 Royal Exchange, Manchester M2 7DB.	55
.30	directions with respect to the longitudinal axis of said plurality of tubes.	Agents for the Applicants	60

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